KRASOVSKIY A. A.

Krasovskiy A. A. and Pospelov G. X., "Certain Methods of Calculating the Approximate Temporary Characteristics of Linear Systems of Automatic Regulation," Avtomatika i telemekhanika, 1953, Volume XIV, No 6, Pages 675-689, 4 tables, 3 illustrations; bibliography, 5 items.

KRASOUSKIY, A.A.

SOLODOVNIKOV, V.V.; professor, doktor tekhnicheskikh nauk, redaktor;
AYZERMAN, M.A., doktor tekhnicheskikh nauk; BASHKIROV, D.A., kandidat
tekhnicheskikh nauk; EROMBERG, P.V., kandidat tekhnicheskikh nauk;
VORONOV, A.A., kandidat tekhnicheskikh nauk, dotsent; GOL'IFARB, L.S.,
doktor tekhnicheskikh nauk, professor; KAZAKEVICH, V.V., doktor tekhnicheskikh nauk; KRASOVSKIV, A.A., kandidat tekhnicheskikh nauk;
dotsent; IERNER, A.Ia., Kandidat tekhnicheskikh nauk; LETOV, A.M.,
doktor fiziko-matematicheskikh nauk; professor; MATVEYEV, P.S.,
inzhener; MIKHAYLOV, F.A., kandidat tekhnicheskikh nauk; PETROV, B.N.;
PETROV, V.V., kandidat tekhnicheskikh nauk; POSPELOV, G.S., kandidat
tekhnicheskikh nauk, dotsent; TOPCHEYEV, Yu.I., inzhener; ULANOV,
G.M., kandidat tekhnicheskikh nauk; KHRAMOY, A.V., kandidat tekhnicheskikh nauk; TSYFKIN, Ya.Z. doktor tekhnicheskikh nauk, professor;
LOSSIYEVSKIY, V.L., doktor tekhnicheskikh nauk, professor, retsenzent;
TIKHONOV, A.Ya., tekhnicheskiy redaktor

[Fundamentals of automatic control; theory] Osnovy avtomaticheskogo regulirovaniia; teoriia. Moskva, Gos. nauchno-tekhn. izd-vo mashino-stroit. lit-ry, 1954. 1116 p. (MLRA 8:2)

1. Chlen-korrespondent AN SSSR (for Petrov, B.N.)
(Automatic control)

SOV/112-58-2-2556

- Translation from: Referativnyy zhurnal, Elektrotekhnika, 1958, Nr 2, p 123 (USSR)

AUTHOR: Krasovskiy, A. A.

TITLE: A Criterion of Quality in a Regulation Process (Ob odnom kriterii kachestva protsessa regulirovaniya)

PERIODICAL: Sb. statey po avtomatike i elektrotekhn. M., AS USSR, 1956, pp 5-10

ABSTRACT: A system of automatic regulation is considered ideal if its transfer function

 $\phi(p) = \frac{a_0 r^n + a_1 p^{n-1} + \dots + a_n}{b_0 p^m + b_1 p^{m-1} + \dots + b_m}$ differs only slightly from the con-

stant $\phi(p) = a_n/b_m$. The ideal system has the amplitude characteristic $\phi(j\omega) \approx a_n/b_m = \text{const}$, and the author suggests that the proximity between a given system and the ideal system be evaluated as the difference between $\phi(j\omega)$ and $\phi(j\omega)$ in the frequency interval $\omega < \Omega$. Let $\phi(j\omega) - \phi(j\omega) < \varepsilon$ in this frequency interval; then ε and ε are, according to the author, the parameters

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SOY/112-58-2-2556

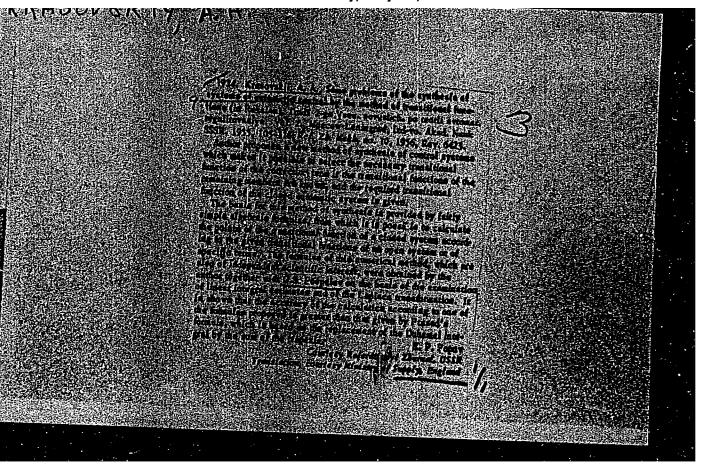
A Criterion of Quality in a Regulation Process

characterizing the quality of regulation. The problem of determining $\mathcal E$ and Ω on the basis of a specified $\Phi(p)$ is reduced to the problem of the distribution of the rocts of two algebraic equations, and it can be solved by Sturm's method. The author points out a simpler but only sufficient condition for the required root distribution, which permits using the conventional stability criteria for determining $\mathcal E$ and Ω . Illustration: 1.

M.A.A.

Card 2/2

"APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000826110



SAVIGH, V.A.; KRASOVSKIY, A.A., redaktor; SHUMIKHIN, K.P., tekhnicheskiy redaktor.

[Psychrometric tables] Psikhrometricheskie tablitay, Leningrad, Oidrometeor. izd-vo. 1957. 251 p. (MIRA 10:11) (Hygrometry-Tables, etc.)

Growth of the public health system in the Komi A.S.S.R. Sov.zdrav.

16 no.10:43-44 0 '57.

(PUBLIC HEALTH, hist.
in Russia)

"APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000826110

KRASOVSKIY, A. A. (Eng. Col.)

(Frof., Dr. Fech. Sci.)

"The Immediate Future of Aviation Automation," Sovetskaya Aviatsiya,
29 June 1957, p. 2.

Sussary - 1156850

KRASOVSKIY, A.A.

"On Two-Channel Automatic Control Systems With Antisymmetrical Bonds," by A. A. Krasovskiy, Moscow, submitted for publication 13 October 1955, Avtomatika i Telemekhanika, Vol 18, No 2, Feb 57, pp 126-136

The article studies linear two-channel systems with asymmetric cross bonds. The classification of asymmetric bonds is presented and transfer functions with complex parameters are introduced. The effect of different symmetric bonds on increasing the stability margin and the critical gain of the system are analyzed. The author holds that two-channel systems are more useful for the synthesis of corrective devices than are single-channel systems. He shows that the introduction of cross bonds provides a considerable enlargement of the stability field.

The author cites a book by R. A. Renkin [name transliterated from Russian], The Mathematical Theory of the Motion of Unguided Rockets, 1951.

APPROVED FOR RELEASE: Monday, July 31, 2000 CIA

CIA-RDP86-00513R000826110(

MULLER, Ferdinand; RUMYANTSEV, Ye.A. [translator]; KRASOVSKIY, A.A., red.

[Remote control] a systematic survey of methods and equipment used in remote control] Teleupravlenie; sistematicheskii obzor metodov i ustanovok teleupravleniia. Moskva, Izd-vo inostr.lit-ry, 1957.

310 p. Translated from the German. (MIRA 14:3)

(Remote control)

KOLOSOV, Sergey Petrovich; SOTSKOV, B.S., prof., doktor tekhn. nauk, retsenzent; KRASOVSKIY. A.A., prof., doktor tekhn. nauk, retsenzent; INOZEMTSEV, S.P., dots., kand. tekhn. nauk, red.; LOSEVA, G.F., red. izd-va; ROZHIN, V.P., tekhn. red.

[Mlements of automatic equipment for aviation] Elementy aviatsionnykh avtomaticheskikh ustroistv. Moskva, Gos. izd-vo obor. promyshl., 1958.

(Airplanes—Hquipment and supplies)

KRASOVSKiy, A.A.

3(4,7)

PHASE I BOOK EXPLOITATION

SOV/2440

- Vsesoyuznyy gidrologicheskiy s"yezd, 3rd, Leningrad, 1957.
- Trudy...t. III: Sektsiya gidrofiziki (Transactions of the 3rd All-Union Hydrological Convention. v. 3: Hydrophysics Section)
 Leningrad, Gidrometeoizdat, 1959. 470 p. Errata slip inserted.
- Sponsoring agency: Glavnoye upravleniye gidrometeorologicheskoy sluzhby pri Sovete Minstrov SSSR.
- Resp. Ed.: V.A. Uryvayev; Ed.: V.S. Protopopov; Tech. Ed.: M.I. Braynina.
- PURPOSE: This work is intended for meteorologists, hydrologists, and hydrophysicists, particularly those engaged in the study of snow and ice and evaporation processes.
- COVERAGE: This book contains papers on hydrophysics which were presented and discussed at the Third All-Union Hydrological Conference in Leningrad, October 1957. The Conference published 10 volumes

-Card 1/14.

Transactions of the 3rd All-Union (Cont.) SOV/2440 on various aspects of hydrology of which this is number 3. editorial board in charge of the series include: V.A. Uryvayev (Chairman), O.A. Alekin, Ye.V. Bliznyak (deceased), O.N. Borsuk, M.A. Velikanov, L.K. Davydov, A.P. Domanitskiy, G.P. Kalinin, S.N. Kritskiy, B.I. Kudelin, L.F. Manoim, M.F. Menkel', B.P. Orlov, I. V. Popov, A.K. Proskuryakov, D.L. Sokolovskiy, O.A. Spengler, A.I. Chebotarev, and S.K. Cherkavskiy. This volume is divided into 2 sections: the first contains reports from the subsection for the study of evaporation processes, and the second contains reports from the snow and ice subsection. References accompany TABLE OF CONTENTS: Foreword 3 List of Abbreviations for Institutions 5 PART I. SUBSECTION OF EVAPORATION STUDY Reports 9 _Card 2/ 14

Transactions of the same		
Transactions of the 3rd All-Union (Com.)	SOV/2440	
Vikulina, Z.A. [Candidate of Geographical Sciences Computing Evaporation From the Surface of Water Res		
GGU Leningrad] Application of the Heat Balance Me mine the Evaporation From the Surface of Water Bodi	natical Sciences, thod to Deter-	
Krasovskiy, A.A. [Director of the Group, Lengidep L plication of GG] and GGO Methods to Determine Evapowater Surface of Reservoirs and the Transpiration of the Group, Lengidep L	eningrad] Ap- ration From the	
Sciences, GGO Leningrad] The Diurnal and Yearly Rattion From Small Bodies of Water	Mathematical te of Evapora-	
Krillova, T.V. [Candidate of Physical and Mathematic GGO Leningrad] Radiation Balance of Water Bodies)ı o	
Vorontsov, P.A. [Candidate of Geographical Sciences grad] Certain Characteristics of Meteorological Con	-	
Card 3/ 14		

3(7) AUTHOR:

Krasovskiy, A. A.

SOV/50-59-1-15/20

TITLE:

The Problem of Calculating Precipitations in Winter (K voprosu

ob uchete zimnikh osadkov)

PERIODICAL:

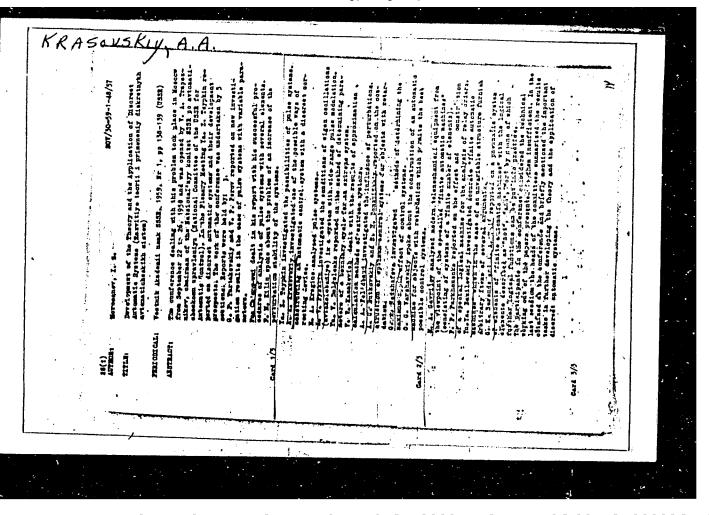
Meteorologiya i gidrologiya, 1959, Nr 1, pp 60-61 (USSR)

ABSTRACT:

A paper by N. V. Razumikhin on the calculation of winterly precipitations in the southern Trans-Volga region is criticized. Snow masses blown into the pluviometer by ground snowstorms are measured although the storms were blowing under a clear sky and precipitations were not real. The daily evaporation from the snow cover is fully neglected on the other hand. This shows that the meteorological service is in a bad way concerning the measurements of winterly precipitations. It would be high time to develop a reasonable method of determining the evaporation losses of the snow cover. There are

1 table and 5 Soviet references.

Card 1/1



S/024/60/000/03/005/028 E140/E463

AUTHOR:

Krasovskiy, A.A. (Moscow)

TITLE:

Dynamics of Continuous Systems of Extremal Regulation

with Random Scanning Signals

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Energetika i avtomatika, 1960, Nr 3, pp 37-45 (USSR)

ABSTRACT: A continuation of the work in Ref 1, where the same

problem was considered for harmonic scanning oscillations in the absence of random fast perturbations. The present

article considers random scanning signals and the

presence of noise. The scanning signal generators give signals assumed independent of each other and of the noise

present. It is further assumed that the random time functions have zero mathematical expectation. The independence condition can also be substituted by the

weaker condition of vanishing of the mathematical

expectations of the products of these random functions. The random scanning signal introduces a small

displacement of the regulated object and the gradient of

the change with respect to the regulated quantity is detected and processed. If it is found that the

Card 1/2

S/024/60/000/03/005/028 E140/E463

Dynamics of Continuous Systems of Extremal Regulation with Random Scanning Signals

displacement results in deviation away from the desired extremal, a correction step is introduced. The precision of the extremal regulation may be analysed by various criteria the simplest of which is the mathematical expectation of the difference $F-F_e$, where F is the function toberegulated and F_e is its value at the extremal. Due to the scanning procedure there is a certain loss of precision even in the absence of noise. The simplest analysis is obtained when the scanning signal is close to white noise. This type of signal also gives the most advantageous results according to the present analysis which, however, neglects the inertia of the regulated object. There are 2 figures and 6 Soviet

SUBMITTED: January 23, 1960

Card 2/2

SOV/24-59-3-7/33

AUTHOR: Krasovskiy, A. A. (Moscow)

TITLE: The Dynamics of Differentiating Continuous-Action Peak-

Holding Systems,

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Energetika i avtomatika, 1959, Nr 3, pp 43-49 (USSR)

ABSTRACT: The treatment relates to systems having relatively few adjustable parameters, and it is assumed that the form of the peak can be approximated by a quadratic equation within the working range of the regulator. Further, it is assumed that phase-sensitive methods are used with small forced deviations provided by a special signal to provide the derivative signals (i.e. the partial derivatives of the output with respect to the adjustable parameters; a separate frequency is assigned to each such parameter). The usual methods of examining stability and transient response in linear systems are then applied. The case in which the various partial derivatives differ greatly in magnitude is considered briefly at the end, in relation to coupled peak-holding systems, i.e. systems in which the rate of change of any one coordinate is

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SOV/24-59-3-7/33

The Dynamics of Differentiating Continuous-Action Peak-Holding Systems

proportional to a linear combination of all the partial derivatives (and not to just one partial derivative). The paper contains 4 figures and 12 references, of which 11 are Soviet and 1 is English.

SUBMITTED: January 12, 1959.

Card 2/2

69892

6.3000

5/109/60/005/04/003/028 E140/E435

AUTHORS:

Krasovskiy, A.A. and Zuykov, V.N.

TITLE:

Limiting Threshold of Sensitivity of Thermal Radio-

Radiation Reception

PERIODICAL: Radiotekhnika i elektronika, 1960, Vol 5, Nr 4,

pp 544-550 (USSR)

ABSTRACT:

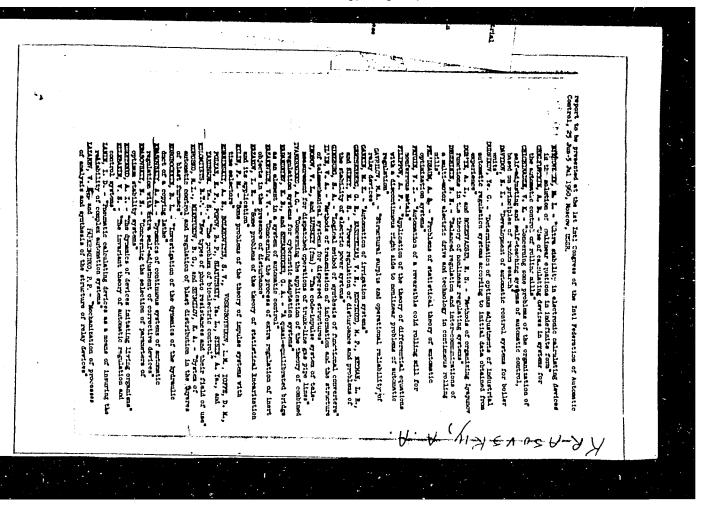
On the basis of Einstein's formula for radiation-energy fluctuations, an expression is obtained for the limiting threshold of sensitivity of thermal radio-radiation 25 receivers. The wavelength brightness temperature plane is divided into two regions. In the first the usual formulae for threshold of sensitivity are valid and in the second region that of short wavelengths and low temperatures, the present formulae are valid. The expressions are valid for arbitrary types of receiver structure (with antenna, absorption cell etc). There are 1 figure and 12 references, 3 of which are Soviet and

9 English.

SUBMITTED:

April 2, 1959

Card 1/1



16,8000

S/194/61/000/002/027/039 D216/D302

AUTHOR:

Krasovskiy, A.A.

TITLE:

Synthesis of self-adjusting automatic control sys-

tems with discrete correcting arrangements

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 2, 1961, 36, abstract 2 V283 (V sb. Teoriya i primeneniye diskretn. avtomat. sistem, M., AN SSSR,

1960, 101-118)

TEXT: The method is given of determining the optimum weighting function of a closed linear system (from the condition of minimum dispersion of error) with discrete correcting arrangement, the transfer function of which secures an optimum transfer function of the whole system. It is assumed that at various instants, spaced by time T, the values of the random component are statistically independent and that the useful component in which the minimization of the deviation, from its optimum, of the real weighting function

Card 1/2

Synthesis of self-adjusting...

S/194/61/000/002/027/039 D216/D302

is achieved by means of varying the parameters of the correcting device. 5 references.

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KRASOVSKIY, A.A.

13.7-000

S/024/60/000/04/007/013 E140/E463 82211

AUTHOR:

Krasovskiy, A.A. (Moscow)

TITLE:

Statistical Dynamics of a System with Proportional Extremal Self-Adjustment of Series Corrective Networks

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Energetika i avtomatika, 1960, No.4, pp.121-129

TEXT: Self-adjustment of corrective networks is required to ensure stability or programme variation of dynamic properties of control systems in the presence of large variations of the characteristics of part of the system. The article considers the dynamics of a system with self-adjustment of series corrective networks consisting of a set of parallel connected filters with variable gain factors. This system is easily realized and in a certain sense is most accessible to theoretical analysis. basis of the system is the comparison of the dynamic properties of the basic open-loop system with those of a certain standard filter. The self-adjustment system is passive if the two sets of properties are identical, but varies the properties of the corrective network in a given manner if a difference exists until that difference vanishes. The variation may be regular or random.

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S/024/60/000/04/007/013 E140/E463 82211

Statistical Dynamics of a System with Proportional Extremal Self-Adjustment of Series Corrective Networks

The case of minimum mathematical expectation of the square of the error in the open-loop system is solved with search signal in the form of white noise. The closed-loop equations are then found. Two forms of the quasi-stationary regime are then examined: the case of strong filtering and a general case, described by non-linear differential equations with random functions as the coefficients. The general case may be solved by a method of successive approximations where the first approximation is the process depends on the degree of filtering in the system. There are 1 figure and 6 references: 5 Soviet and 1 English.

Card 2/2

82940

16,9500

S/103/60/021/009/008/013 B012/B063

AUTHOR:

Krasovskiy, A. A. (Moscow)

TITLE:

The Theory of Two-channel Servo-systems With a Relay

Element in the Alternating-current Circuit

PERIODICAL:

Avtomatika i telemekhanika, 1960, Vol. 21, No. 9,

pp. 1293-1305

TEXT: The present article describes a comparatively general method of investigating two-channel servo-systems with relay elements in their alternating-current circuits. Some of their common properties are mentioned, and it is noted that the method given here is convenient for the solution of concrete problems. The above-mentioned two-channel servo-system is schematically shown in Fig. 1, and an appendage to the present paper contains the complete system of equations (4) of the transfer functions. The relay systems of this type mainly operate with self-oscillations. To determine stabilized self-oscillations, the solution of system (4) is sought in the form of (5). The kind of this approximate solution corresponds to the method of harmonic equilibrium (Ref. 4). If this method Gard 1/3

The Theory of Two-channel Servo-systems With a Relay Element in the Alternating-current Circuit

82940 S/103/60/021/009/008/013 B012/B063

is applied to two-channel systems with modulation and a non-linear element in their alternating-current circuit, it becomes an exact method for the determination of self-oscillations in the case of unbounded increase of the carrier frequency. This is achieved by neglecting the harmonics of the carrier frequency Ω or the combined frequency $\Omega \pm \omega_a$ instead of the

harmonics of the self-oscillation frequency ω_a . In this connection the nuther refers to a paper by L. S. Gol'dfarb (Ref. 4). The stability of self-oscillations according to Lyapunov is investigated next. An approximate equation (13) is derived for the deviations of self-oscillations, and an approximate criterion is formulated for the stability of self-oscillations in the above-mentioned systems having relay elements. It is shown that this criterion follows formula (13). The author determines the transfer function of the system linearized by self-oscillations with respect to slow central actions. It is noted that the characteristic equation (22), which corresponds to the transfer function in the case of slowly varying input quantities, agrees with equation (13) up to

Card 2/3

82940

The Theory of Two-channel Servo-systems With a Relay Element in the Alternating-current B012/B063

one summand. This indicates that, if there are stable self-oscillations, self-oscillating servo-systems are analogous to stable, linear systems as far as the reproduction of slowly varying input quantities is concerned. In the self-oscillating relay systems under discussion, the reaction to slow disturbances is independent of the absolute value of the amplification factor of the open circuit. Finally, it is said that the abovedescribed method may be applied to relay elements having hysteresis and an insensitive range. There are 5 figures and 8 Soviet references.

SUBMITTED: November 19, 1959

4

Card 3/3

5/024/61/000/001/003/014 E197/E435

AUTHOR:

Krasovskiy, A.A. (Moscow)

TITLE:

Certain conditions for the application of self adjusting

systems in automatically controlled continuous

productive processes

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Energetika i avtomatika, 1961, No.1, pp.97-109

TEXT: The author examines general schemes of continuous production systems in which the controlling devices, such as drives, plant and regulators which control the process, are set automatically. principle is based on obtaining a quality index of production and keeping it within certain limits and utilizes the natural fluctuations of the parameters of production superimposed by quality searching oscillations where advisable. Such self adjusting processes are analysed in an approximate, qualitative The essential conditions and requirements of a control loop are postulated, both with respect to the self adjustor and to the automated process itself. The author prescribes that there shall be a number of adjustments on the machines, tools, equipment and regulators which control the manufacturing process. Card 1/4

S/024/61/000/001/003/014 E197/E435

Each of these has some sort of adjustment which is suitable to be set to produce a certain quality and quantity of a product. Simultaneously with the planned adjustment of the process, various other factors will tend to upset the required quality index, such as variation in the raw materials, wear and tear, change of temperature, perturbations in production variables and the like. The effect of the main disturbing factors should be capable of being expressed precisely in terms of a change in the set point of the control elements. The author introduces the term "period of misalignment", meaning the time period for which the product remains within specified limits with no change in set points. self-adjusting systems that period must be very long in comparison For with the response time to plant disturbances. It is further postulated that any output parameter shall be dependent on one adjustment only, if there should be no interaction between loops. The plant will be subject either to perturbations inherent in the system or to induced perturbations. Self-adjustment is accomplished by correlating the measured perturbations with their effect and by a network of delay lines precisely equivalent to the delay prevailing in the manufacturing process itself. Card 2/4

Certain conditions ...

S/024/61/000/001/003/014 E197/E435

system was first proposed and realized by A.B.Chelyustkin (Ref.3: Application of Computers to Automatic Control Systems in Rolling Mills, Proceedings of IFAC, 1960). In general, the minimum time needed for an effective self-adjustment will be 4 to 6 times the process lag. The author arrives at the following conclusions. A satisfactory transient response of the self-adjustment processes can be achieved if the magnitude of the controlled high-frequency search oscillations is sufficient for unambiguous separation of the desired component of the correlator signals for given storage times. 2. When the automatic-adjustment system of the equipment is switched on, the time of self-adjustment should be less than the misalignment time when the positions of the adjustment organs remain fixed. 3. The self-adjustment time should exceed the delay time of the production - quality control and the signal storage time. 4. Low-frequency components of the errors of the production parameter control, whose correlation times exceed the self-adjustment times, introduce parameter errors of the same order as the control errors and should satisfy the corresponding tolerances. 5. The higher the level of the primary automation of a production process the longer will be the Card 3/4

Certain conditions ...

S/024/61/000/001/003/014 E197/E435

misalignment time (other conditions being equal) and the more successful the automatic-adjustment control systems for production processes. There are 2 figures and 6 Soviet references.

SUBMITTED: October 29, 1960

Card 4/4

30555 **\$/569/61/002/**000/008/008 **D29**8/**D302**

16.8000 (1031, 1132, 1329)

AUTHUR:

Krasovskiy, A.A. (USSR)

TITLE: Dynamics of continuous systems with extremum self-

adjustment of compensating networks

SOURCE: IFAC, 1st Congress, Moscow 1966. Teortya diskretnykh,

optimal'nykn i samonastraivayushchikhsiya sistem.

Trudy, v. 1, 1961, 962 - 977

TEXT: The first-approximation integro-differential equations are derived for continuous systems with extremum adjustment of compensating networks. It is shown that for quasistationary conditions, these equations degenerate into the equations of an extremal continuous system. The stability conditions are stated for the quasistationary process. By another work of the author (which is in print), control systems with adaptive compensating networks are divided into 3 groups: 1) With open loop compensating networks; 2) With closed-loop compensating networks, and 3) With extremum adjustment of compensating networks. In system 3), values of the pacard 1/7

30555 3/569/61/002/000/008/008 D298/D302

Dynamics of continuous systems ...

rameters of the compensating network are searched which correspond to the extremum of the performance criterion of the process and to stabilization; the performance criterion is a functional of the parameters of the compensating network. A block diagram of the system is shown. The square deviation ϵ^2 is a measure of the different ce of response, to the control signal θ , on the part of the control system Φ (which contains the compensating network, the controller, and the plant) and the reference fixter Φ_0 , respectively. The quantity ϵ^2 is applied to m synchronous detectors, where the search oscillations δx_1 , δx_2 , ..., δx_m arrive as well. From the configuration it is evident that the process of parameter self-adjustment will continue as long as the quantity ϵ^2 has components which are synchronous with search oscillations. These components vanish only at the extremum (minimum) point of a certain mean value of ϵ^2 . The adjustment process depends largely on the form of the control signal e. If 0 does not provide in itself a sufficiently regular adjustment, additional random- or regular signals have to be applied to the system input; in the following, 8 in conjunction with the Card 2/7

30555 \$/569/61/002/000/008/008 D298/D302

Dynamics of continuous systems...

additional signals, will be called the test signal 0. The test signal, as well as the search oscillations are assumed to be random (in the general case - non-stationary) functions of time; the results can be readily extended to regular test- and search signals. It is assumed that the weight (impulse) function K of the principal loop is analytic with respect to the adjustment parameters x_i, viz.

$$X_{l} = X_{l} + \Delta x_{l}$$

$$K(l, \tau, x_{l}) = K(l, \tau, X_{l}) + \sum_{l=1}^{m} \frac{\partial K}{\partial x_{l}} \Delta x_{l} + \frac{1}{2l} \sum_{l=1}^{m} \sum_{l=1}^{m} \frac{\partial^{2} K}{\partial x_{l}^{-1} v_{l}} \Delta x_{l} \Delta x_{l} + \dots;$$

$$(1)$$

the output variable ε is related to the input variable θ by the equation

 $\varepsilon' = \int_{-\infty}^{\infty} K(t, \tau, x_i) \theta(\tau) d\tau.$ $\varepsilon' = \int_{-\infty}^{\infty} K(t, \tau, x_i) \theta(\tau) d\tau \int_{-\infty}^{\infty} K(t, \tau, x_i) \theta(\tau) d\tau =$ $= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} K(t, \tau_1, x_1(\tau_1)) K(t, \tau_2, x_1(\tau_1)) \theta(\tau_1) \theta(\tau_1) d\tau_1 d\tau_2.$ (2)

Card 3/7

Hence

APPROVED FOR RELEASE: Monday, July 31, 2000

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Dynamics of continuous systems ...

The mathematical expectation of the output variable of a linear operator, equals the operator of the expectation; hence

$$X_{i} = \frac{V_{F}}{D} M(\epsilon^{2} \delta x_{i}), \qquad (4)$$

where $X_i = M(x_i)$ is the mathematical expectation of the i-th parameter, and $W_F(D)$ is the transfer function of the filter. Two simplifying assumptions are made: a) the dispersion of W/D δu_i (u being a random function) is much smaller than the dispersion of δx_i , and b) only the first two terms of series (1) are retained. Hence one obtains the first-approximation integro-differential equations:

$$DX_{i} = 2W_{\underline{\sigma_{i}}}(D) \times \times \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} K[t, \tau_{1}, X_{i}(\tau_{1})] \frac{\partial}{\partial X_{i}} K[t, \tau_{2}, X_{i}(\tau_{2})] R_{\delta_{i}}(\tau_{2}, t) R_{\delta}(\tau_{1}, \tau_{2}) d\tau_{1} d\tau_{2}.$$

$$(i = 1, 2, \ldots, m)$$

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Dynamics of continuous systems ...

(R is the correlation function). These are general equations which apply to both stationary—and non-stationary ox, and w, and cover many particular cases, as for example: 1) The correlation time of

many particular cases, as for example: 1) The correlation time of the search signals is much larger than the time of the transient processes in the principal loop. 2) The test signal is a white noise. 3) The test signal and the search signal are stationary. In addition, the case of quasi-stationary conditions is considered in more detail. In this case, Eq. (9) becomes

$$DX_{i} = \overline{\delta^{2}x_{i}} W_{p}(D) \frac{\partial}{\partial X_{i}} \overline{e^{2}}(q, X_{1}, X_{2}, \dots, X_{m}), \tag{13}$$

where $\overline{\varepsilon^2}(q, X_1, X_2, \ldots, X_m) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} K(t-\tau_1, X_1, q) K(t-\tau_2, X_1, q) R_{\theta}(\tau_1, \tau_2) d\tau_1 d\tau_2$

(after setting $\overline{\delta^2 x_i} = \text{const}$). Eq. (13) is analogous to the equations of a continuous system of extremum control by the method of gradient (considered in an earlier work by the author). The notation $W_F(D) = -aW(D)$ is introduced, where W(D) is the normalized Card 5/7

30555

\$/569/61/002/000/008/008 D298/D502

Dynamics of continuous systems ...

transfer function. In the case of quasi-stationary self-adjustment with white-noise test-signal, one obtains:

$$DX_{i} = -\alpha V(D) \frac{\partial I}{\partial X_{i}}$$
 (15)

where I is the integral square estimate of K. For linear systems with lumped parameters, the derivatives $\partial I/\partial X_i$; $\partial^2 I/\partial X_i \partial X_j$ can be found analytically. The quasi-stationary process is stable if the minimum condition

$$X_{1} = X_{e}; \frac{\partial I}{\partial X_{1}} = 0; (i = 1, 2, ..., m)$$

holds, the m roots of

$$\begin{vmatrix} \lambda - a_{11} & a_{12} & \dots & a_{1m} \\ a_{21} & \lambda - a_{22} & \dots & a_{2m} \\ \vdots & \vdots & \ddots & \vdots \\ a_{m1} & a_{m2} & \dots & \lambda - a_{mm} \end{vmatrix} = 0, \tag{16}$$

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Dynamics of continuous systems ...

are positive, and the lag of the filters is negligible. A discussion followed. Taking part were: V.N. Varygin, Tarasov, I.Ye. Kazakov, R.I. Stakhovskiy (USSR), A.Straszak (Poland). There are 3 figures, and 7 references: 5 Soviet-bloc and 2 non-Soviet-bloc (in translation.)

V

Card 7/7

S/588/61/000/004/001/011 D234/D303

/6.8000 AUTHOR:

Krasovskiy, A.A.

TITLE:

Principles of search and the dynamics of continuous

systems of extremum control

SOURCE:

Avtomaticheskoye upravleniye i vychislitel naya

tekhnika, no. 4, Moscow 1961, 5 - 49

TEXT: The first part of the article is a survey of the principles of search. The following subjects are considered: Examples of systems of extremum control; methods of extremum search (synchronous detection during harmonic oscillations of search, for determining the gradient; method of time derivative for the same purpose; method of extremum memorizing; Gauss-Seidel method of alternating changes of variables; method of the gradient; method of quickest descent); structure of the systems. The second part deals with the dynamics of many-dimensional systems of extremum control in case of regular or random search signals and is based on previous publications of the author. There are 20 figures and 20 references: 19

Card 1/2

Principles of search and the ...

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Soviet-bloc and 1 non-Soviet-bloc. The reference to the English-language publication reads as follows: S. Drapper and I.T. Li, Principles of optimalizing control systems and an application to internal engine. ASME publications 1951.

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Cara 2/2

89170

\$/103/61/022/002/001/015 B104/B201

16.9500 (1031, 1121, 1132) AUTHOR:

Krasovskiy, A. A. (Moscow)

TITLE:

4

Antisymmetric feedback two-channel servosystems with random

disturbances

Avtomatika i telemekhanika, v. 22, no. 2, 1961, 143-156 PERIODICAL:

TEXT: In Refs. 1 and 2 the author has studied two-dimensional linear systems and relay systems with antisymmetric feedback in the presence of a regular control and random disturbances. The statistical dynamics of similar systems is examined in the present paper. The first part is devoted to linear stationary systems with complex transfer functions which are under the influence of random disturbances. Fig. 1 shows a block diagram relative to such systems, in which the antisymmetric feedbacks are indicated by dotted lines. The complex input quantity of this system is expressed by the relation $\overline{x}_{in} = x_{in}^! + jx_{in}^n$ and the noise $\overline{f}_0 = f_0^! + jf_0^n$. Caused by $\overline{x}_{in}^!, \overline{f}_0$, the disturbances $\overline{f}_i = f_i^! + jf_i^n$ (i = 1,...,) act upon the various points of the system, and $\overline{x}_{in}^!, \overline{f}_0$, and \overline{f} are regarded as independent Card 1/5

89170

Antisymmetric feedback two-channel...

S/103/61/022/002/001/015 B104/B201

continuous random functions. Thus, all these functions may be represented as $x_{in} = W_{in}g_{in}$, $f_i = W_{fi}g_{in}$, (i = 0,1,...,y) (1), where W_{in} and W_{fi} denote complex transfer functions of the so-called shaping filters, \overline{g}_{in} and \overline{g}_{i} are independent random functions with a constant spectral density (white noise). With reference to his previous studies the author finds expressions for the pulse-transfer functions and obtains the following expression for the error $\overline{\Delta x} = x_{out} - \overline{x}_{in}$:

$$\overline{\Delta x} = -\frac{W_{in}}{1+W}\overline{g}_{in} + \frac{WW_{fi}}{1+W}\overline{g}_{0} + \sum_{i=1}^{W}\frac{W_{i}W_{fi}}{1+W}g_{i}$$
 (3), where W denotes the

complex transfer function of the open circuit, W_i is the transfer function from the ith input to the output. The pulse-transfer function of a two-channel system can be described as follows: $\overline{k}(t) = k'(t) + jk''(t)$, and it is shown that the generalized complex transfer functions of the system investigated correspond to the transfer functions in the expression (3): $\overline{k}(t) \dots - \overline{w}_{in}/(1+\overline{w})$, $k_i(t) \dots ww_{fi}/(1+\overline{w})$, $(i = 0, 1, \dots, \nu)$.

Card 2/5

Antisymmetric feedback two-channel...

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Proceeding from these results, the author passes over to the representation of the input quantities of the system by complex weight functions (transfer functions), and discusses an estimation made for the weight functions. The second part deals with servosystems with relays in the a-c channel and a two-channel section possessing an infra-low frequency. The system shown in Fig. 4 and already examined in a previous paper, is taken as a basis. Regarding the expected mathematical value, the principal mode of operation of this system is shown to be its natural oscillation. The production of natural oscillations in this system is discussed, and the equivalent circuit shown in Fig. 9 for the system considered is discussed thoroughly. This equivalent circuit reproduces the statistical dynamics of the system accurately in the case of white noise, and by approximation in the case of any noise with Gaussian distribution. A thorough investigation of a suppression of the noise in the relay element shows that it has an effect solely upon such an amplitude of oscillations as considerably exceeds the mean square root of the noise. It is further shown that the oscillations possess a determined frequency and can therefore be filtered with suitable circuits without modifying the dynamic properties of the entire system. There are 11 figures and 9 Soviet-bloc references.

Card 3/5

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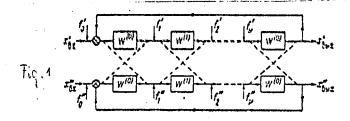
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Antisymmetric feedback two-channel...

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SUBMITTED: May 24, 1960

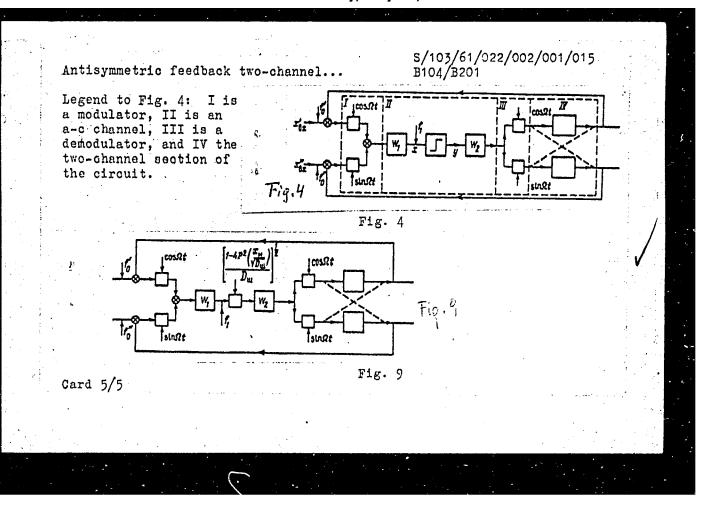
Legend to Fig. 1: $x_{\delta X}^i$ and $x_{\delta X}''$ correspond to x_{in}^i and x_{in}^u , $x_{\delta u X}^i$ and $x_{\delta u X}^u$. correspond to x_{out}^i and x_{out}^u .



Card .4/5

APPROVED FOR RELEASE: Monday, July 31, 2000

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%771 S/103/61/022/006/006/014 D229/D304

AUTHOR:

1.4400

Krasovskiy, A.A. (Moscow)

TITLE:

Extremum reception of signals

PERIODICAL: Avtomatika i telemekhanika, v. 22, no. 6, 1961,

730 - 738

TEXT: The author considers a principle of extremum recontion which is as follows: The signal received consists of a useful component f and a disturbance f the general form of the former is supposed to be known and is characterized by some parameters, such as amplitude, frequency, duration and phase of pulses etc. The signal is compared with that of an automatically tuned internal generator f, the generator being so designed that the difference f f can be made arbitrarily small. The difference between the received and the generater signal is sent to a difference estimation unit, the output quantity of which is sent to an optimizer - a system of

Card 1/2

26771 5/103/61/022/006/006/014 D229/D304

Extremum reception of signals

extremum regulation which secures the finding and realization of generator tuning that gives minimum estimation of the deviation. The useful output signal of the system is that of the generator, or only the parameters of the tuning. The method of search is the gradient method. The author deduces the system of equations of extremum reception which are non-linear, and formulates the assumptions for quasi-stationary reception under which the equations become linear. No analysis of consistency of the assumptions is made, but it is claimed that these are consistent for several specific cases. A characteristic equation of stability of extremum reception under these assumptions is given. The possible stability against disturbances is found to be equivalent to that of the correlation reception, but the latter requires exact previous realization of carrier functions in the receiver while extremum reception does not. This constitutes the chief advantage of the latter. An example is studied in detail. There are 4 figures and 6 Sovietbloc references. SUBMITTED: August 30, 1960

Card 2/2

KRASOVSKIY, A. A.

"Optimal Searching Techniques for Control Sampled Data Extremum Control Systems."

Presented at IFAC International Federation of Automatic Control Symposium on Self Adjusting System Theory, Rome 26-28 Apr 62

KRASOVSKIY, Aleksandr Arkad'yevich; POSPELOV, Germogen Sergeyevich; KOROLEV, N.A., red.; BUL'DYAYEV, N.A., tekhn. red.

[Principles of automatic control and engineering cybernetics]
Osnovy avtomatiki i tekhnicheskoi kibernetiki. Moskva, Gosenergoizdat, 1962. 599 p.

(Cybernetics) (Automatic control)

KPASOVSKY, A. A.

"Problems in the Theory of Continuous Systems of Extremum Process Control."

 $^{p}\mathrm{aper}$ to be presented at the IFAC Congress held in Basel, Switzerland, 27 Aug to h Sep 63

AM1037979 s/ BOOK EXPLOITATION Krasovskiy, Aleksandr Arkad'yevich Dynamics of continuous self-adjusting systems (Dinamika neprery*vny*kh samonastraivayushchikhsya sistem), Moscow, Fizmatgiz, 1963, 468 p. illus., biblio., index. 8,000 copies printed. TOPIC TAGS: automation, computer engineering, continuous self adjusting system, continuous extremal regulation TABLE OF CONTENTS [abridged]: Foreword -- 7 Ch. I. Information in control processes and self-adjusting systems -- 9
Ch. II. Examples of continuous self-adjusting automatic control systems -- 26 Ch. III. Methods of seeking the extremum -- 82 Ch. IV. Dynamics of continuous extremal regulation -- 159 Ch. V. Forced processes of extremal regulation -- 238 Ch. VI. Synthesis of continuous extremal regulation systems -- 282 Ch. VII. Solf-adjusting control systems for continuous production processes -- 304 Card 1/2

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	Ch. IX. Stabilization of Ch. X. Extremal systems o	dynamic characteristics of automatic regulation 375 f stabilization and optimization of the dynamic	
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KRASOVSKIY, A.A. (Moskva)

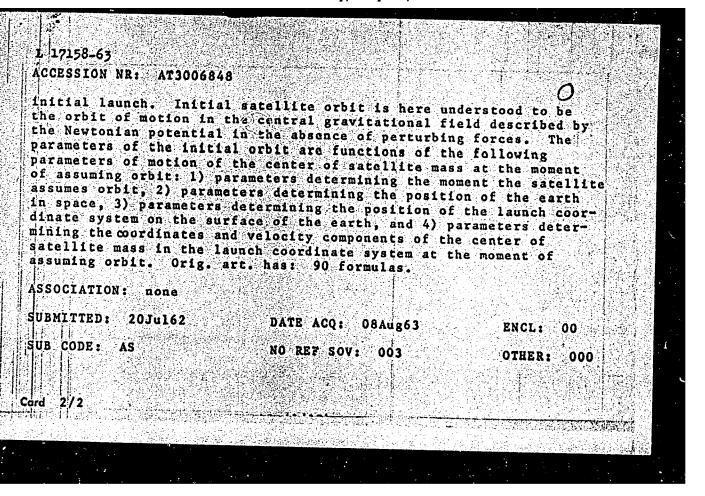
Entropy stability of linear continuous automatic control systems.

Izv. AN SSSR. Tekh. kib. no.5:19-26 S-0 '63. (MIRA 16:12)

14.34 L 17158-63 EPA(b)/EVT(1)/ICC(v)/FS(v)-2/BDS/ES(v)AFFTG/AFFDC/ ESD-3/APGC/SSD Pd-4/Pe-4/Pg-4/Pq-4 GW ACCESSION NR: AT3006848 5/2560/63/000/016/0211/0225 AUTHOR: Aleksakhun, I. V.; Krasovskiv, A. A.; Lebedev, Yakovleva. A. I. TITLE: Determination of the parameters of the initial orbits artificial earth satellites SOURCE: AN SSSR. Iskusst. sputniki Zemli, no. 16, 1963, 211-225 TOPIC TAGS: satellite orbit, orbital element, satellite launching, coordinate system, initial orbit, orbital parameter, rocketry ABSTRACT: Based on the theory of undisturbed planetary motion, working formulas have been obtained for computing: 1) the parameters of the initial orbit based on given parameters of the motion of the center of satellite mass at the moment of going into orbit, and 2) partial derivatives from the parameters of the initial orbit on the basis of the parameters of motion of the center of satellite mass in the launch and initial launch coordinate systems at the moment of going into orbit. Four Cartesian rectangular coordinate systems are employed, i.e., launch, ground, sidereal, and Card 1/2

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000826110



KRASOVSKIY, A.A. (Moskva)

Quasi-stationary process in continuous optimalizing control with coordinate limitation. Avtom. i telem. 24 no.12:1633-1642 D '63. (MIRA 17:1)

NIKOLAYEV, Andrey Grigor yevich; PERTFOV. Sergey Viktorovich;
PERESLEGIN, S.V., retsenzent; FEDIN, V.T., retsenzent;
KRASOVSKIY. A.A., prof., doktor tekhn.nauk, nauchn. red.
MASHAROVA, V.G., red.

[Radar detection of thermal radiation; passive radar] Radioteplolokatsiia; passivnaia radiolokatsiia. Moskva, Sovetskoe radio, 1964. 334 p. (MIRA 17:12)

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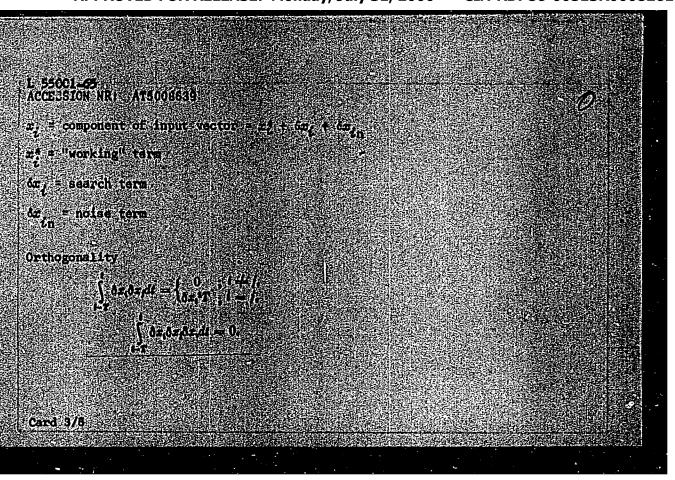
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article only problems in which the Aprovalinformation of the object is a wintmum are considered, so where nothing is known about the characteristics of the
object. In continuous and sampled data optimalizing control systems the composnents of the gradient of the function F which expresses the characteristics of
the object are taken as a measure of the deviation from the optimum. The optimum
linear operator is that which guarentees the greatest precision in determining
the components of the gradient ima given time interval. It is shown that the
optimum operation for determining the components of the gradient from the class
of all realizable linear operators, is synchronous detection of the form

when the following conditions are men

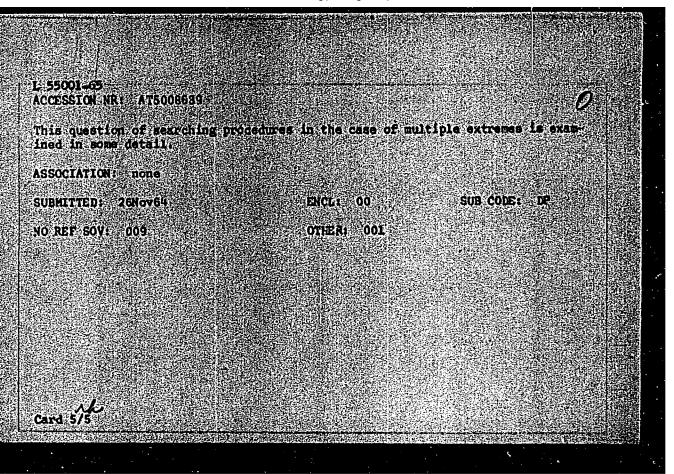
$$\left(\sum_{i=2}^{n}(e^{2it}e^{2it})\right)$$

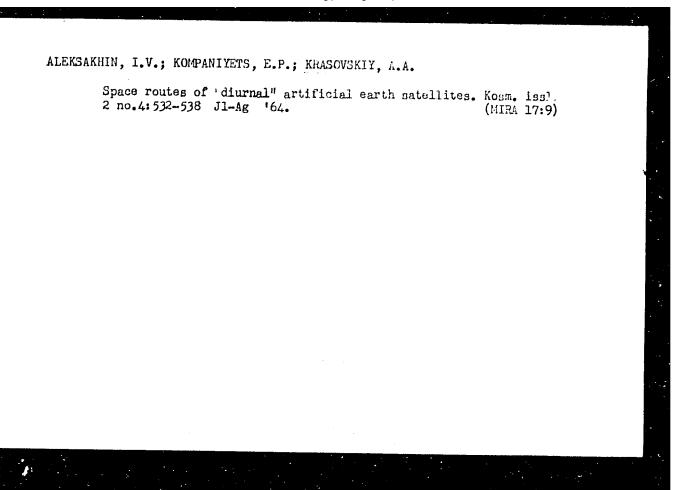
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Constant values of input working coordinates (at a const. during integration time	
\(\sum_{0}\) \(\delta_{0}\) \(\delt	
$R(\tau,\tau) < F_{\bullet}(\tau) + \delta F_{\bullet} (F_{\bullet}(\tau) + G_{\bullet} _{L^{2}})$	
where R is the correlation function: In accordance with this proof the mentioned conditions are sufficient but not all are necessary. Therefore the general condi-	
tions for optimality of synchronous detection as illustrated in the mathod for determining the components of the gradient are obviously broader than in the case given here. In many cases the extremal equation of the characteristics of the	
object F(x, x, x) have several extrema from which the one corresponding to some oriterion must be selected, e.g. that having the greatest absolute value. The complex nature of F and the presence of several extrema may have the same	
significance in the control of real industrial objects, as in the solution of the problem of the automatic synthesis of control systems with the aid of an optimizer	
Card 4/5	

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1. 19867-65 BF(d) FG-L/PG-L/PS-L/PS-L/PL-L I.P(c)/ASD(s)-5/AFD(p)/SD(d)

ACCESSION NR: AP4048819 8/0880/64/000/005/0003/0018

AUTHOR Krasovskiy A.A./(Neccor)

TILE Entropy change in continuous dynamic systems

SOURCE AN SSR. Ixy Technicheskays libernetiks, No. 5, 1964, 3-16.

TOPIC TAGS: sutomation, control system entropy, continuous dynamic system, random perturbation

ABSTRACT. This article is a continuation of the author's previous work on the entropy of control systems (Isy AN SSR, Technicheskays Kibernetika, 1963, No. 5); only now the effect of random external perturbations is taken into account. Two types of entropy are considered; macroentropy or entropy in the decal information theory sense, i.e. a measure of uncertainty in the macrococordinates of the system, and microentropy or entropy in the decal information theory sense, i.e. a macroentropy of an arbitrary nonlinear dynamic system, subject to random perturbations, is derived. The total microentropy due to the macrocordinates of a linear passive system with reactive coupling is derived by proving the following theorem:

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H= (and kr) = 1	
	0)
where the moment matrices satisfy the equations	
mlique FIE clique FIE [m] and [c] are determinants of system coefficient matrices;	(3)
W-IKIGGIL KE-IKIGAJI.	(6)
[E] is the unit matrix; of is the generalized system coordinate and u is the number ments (loops) in the system, whose temperature T is assumed to be equal. If a co	of ele- lection
Card 2/4	

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of Lagrangian elements) each having one degree of freedom and describable by

$$m_{ij}(q) + r_{ij}(q) + r_{ij}(q) = P_{ij} + (i = 1, 2, \dots, n), \tag{4}$$

where $P_{\rm L}$ is the generalized forcing function, are coupled by active or passive means by letting

then the system

$$m(q) + c_1q(1+c_1q) - P(q_1q_2, \dots, q_r) = 0$$

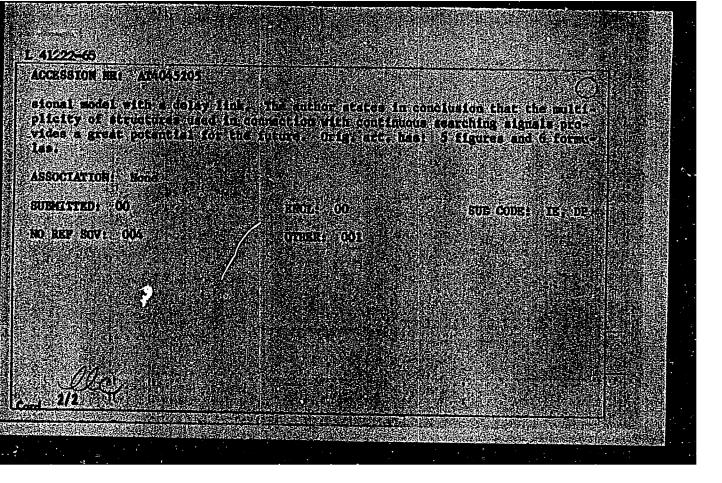
is called a semilinear isolated system with Lagrangian elements and its macroentropy is only due to random mittal conditions. It is shown that for such system the sum of the

Card: 3/4

L 19867-65 ACCESSION NR. AP4048819 macroentropy. If and of the half-microentropy He is always constant. Half for one sec tion is defined by $\alpha_{ij} = \alpha_{ij}/2\nu_{ij}$ (5) where dQ, is the amount of nest repaired by the element and U, is its kinetic energy (or equivalent). When 21/2 kl, the total increase dH, becomes proportional to the entropy increase in the thermodynamic sense. It is concluded that in order to assure the entropy stability of systems with lagranging elements; it is necessary to have elements which can radiate heat. An ordering of the macrosystem is accompanied by an increase in half-microentropy. It is thus required to have not only the necessary regulatory devices but also a medium whose half-microentropy can increase. Orig. art has: 42 equations and 3 figures ASSOCIATION: None SUBMITTED: 15 Feb84 encli- 00 SUB CODE: IE TD NO REF SOVE 006 OTHER 2000 Card 4/4

-FE (6)/FE (E)/FE (L)/FE //FE //FE (U) - T. the tector 41222-65 19/2:58e/(44/000/006/0054/0063 **LYXIO** \$205 ACCESS TOR INC. AUNDER Tractive Lyche An System 2 (0 3 Cat process to make a father and on of the opinion of control to regard THE STATE OF THE S ATTOMATICINALIONE UPLAYIGITIES ATTOMISED LOUVE TOUBLE, no. 6, 1904 SOURCE: 54-63 TOPIC-TAGS: Information processing opermet control, electrosimilation, control mode L ABSTRACT: The suther; points out the the arficle that for the greatest scouracy of the information processing evaluations of the sufferential being application of verticus data on the tests of the section of the sufferential on the tests of the section of the sufferential on the tests of the section of the sufference of the source of the section of

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SCURCE: Avtomatika 1 (élémékinn	1km, 1, 26, no. 5, 1965, 545-547
TOPIC TAUS: Gynemic system; non	linear dynamic system
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aya tems described a by of faren	fons of the general entropy stability for the training of the first and neth orders are seen copy-stable but still unstable in the has 19 formulas.
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ACCESSION | pr Alegal No. | UNIOSEN/65/080/051/00218

AUTION: LeavyLis Air Air (N-25)/2

TITLE: Brak istical spublicy of billing objectives dynamic systems and integral sestimates of moments

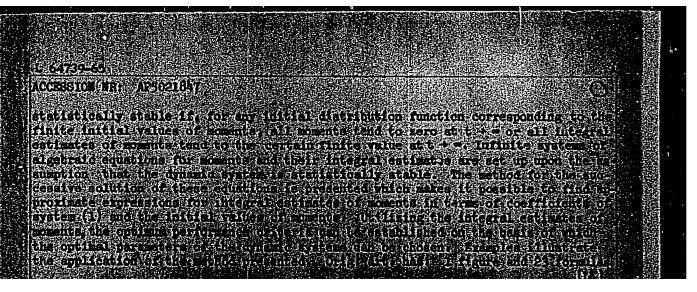
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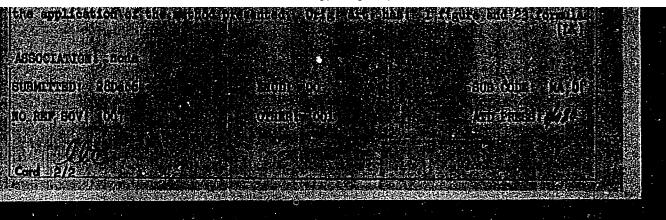
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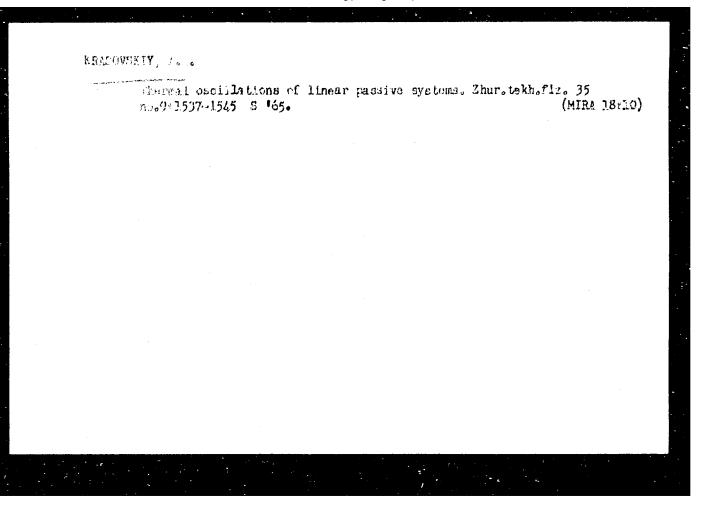


"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000826110

AUTHOR: Krasovskiy, A. A. (Moscow) TITLE: Linear passive systems subjected to internal thermal noise ? SOURCE: Avtomatika i telemekhanika, v. 26, no. 6, 1965, 1026-1036 TOPIC TAGS: linear passive system, thermal noise ABSTRACT: An intrinsic-thermal-noise correlation-matrix theorem is suggested for any linear passive system describable by the Lagrange equations and existing in a state of thermal equilibrium (all system components have the same temperature). The proof is based on a special postulate of thermal-noise spectral-density matrix and on V. S. Pugachev's equations describing the moments of a system subjected to white noise (Trans. of VVIA, no. 18, 1944). General formulas are developed for dispersions, cross moments of macro-coordinates, and entropy, and also for mean cancillustrate the use of the above formulas: maximum random drift of a gyroscope operating in a viscous medium, thermal noise in a multiwinding transformer, thermal vibrations of a string galvanometer. Orig. art. has: 4 figures and 80 formulas.	L ^C 0812-66 EEO-2/EWT(1)/EEC-l ₁ /EED-2/ LCCESSION NR: AP5015906	EWA(h) ESD JM UR/0103/65/026/006/1026/1036	
SOURCE: Avtomatika i telemekhanika, v. 26, no. 6, 1965, 1026-1036 TOPIC TAGS: linear passive system, thermal noise ABSTRACT: An intrinsic-thermal-noise correlation-matrix theorem is suggested for any linear passive system describable by the Lagrange equations and existing in a state of thermal equilibrium (all system components have the same temperature). The proof is based on a special postulate of thermal-noise spectral-density matrix and on V. S. Pugachev's equations describing the moments of a system subjected to white noise (Trans. of VVIA, no. 18, 1944). General formulas are developed for dispersions, cross moments of macro-coordinates, and entropy, and also for mean canetic and potential energies of system thermal fluctuations. These examples illustrate the use of the above formulas: maximum random drift of a gyroscope operating in a viscous medium, thermal noise in a multiwinding transformer, thermal vibrations of a string galvanometer. Orig. art. has: 4 figures and 80	내 불물이 들고 그렇게 되고 아무리 사람이 바람이다.	62-501.1	
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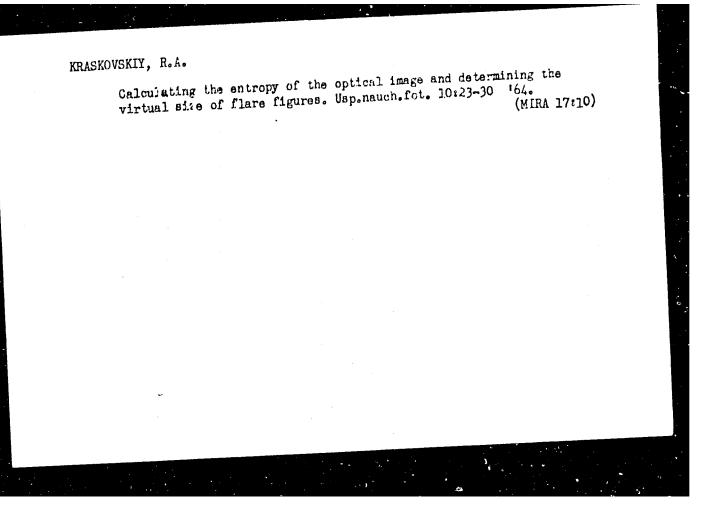
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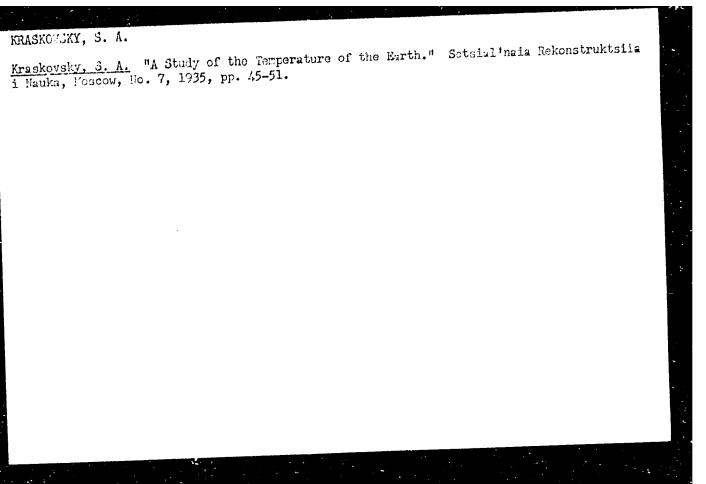
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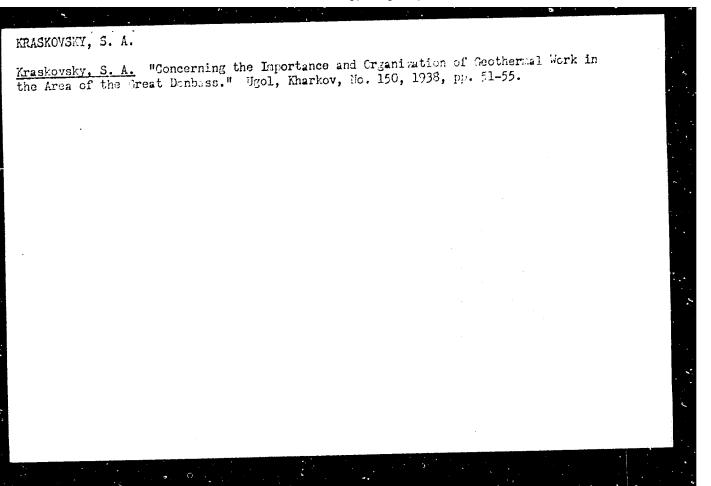
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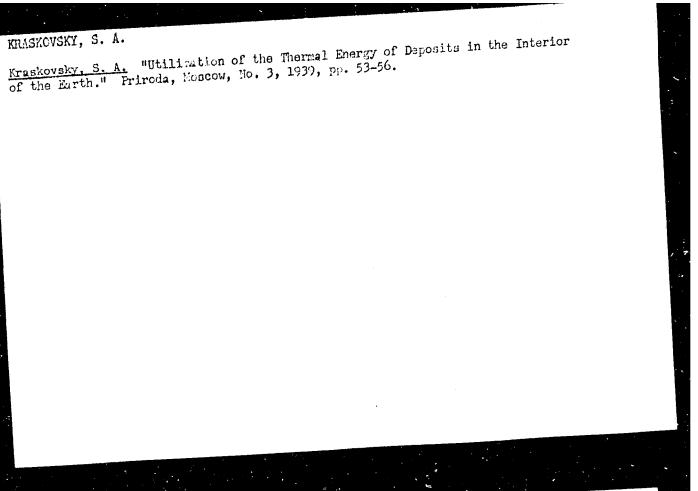
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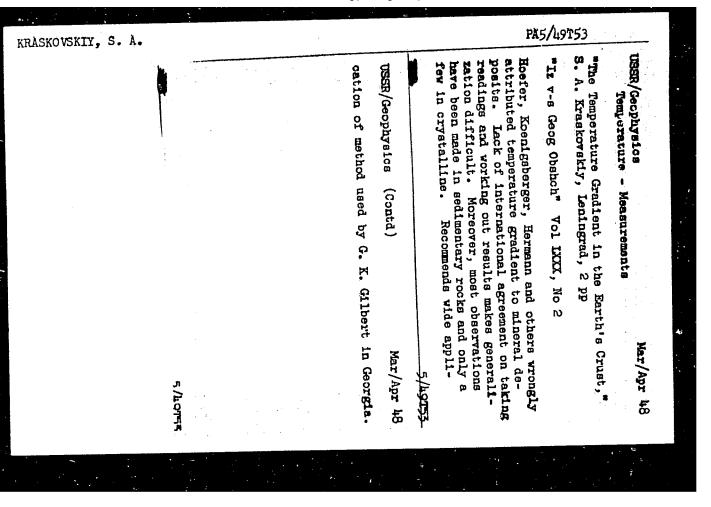


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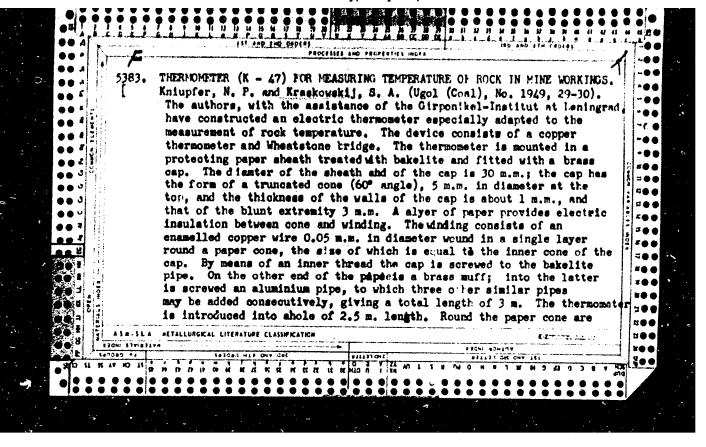
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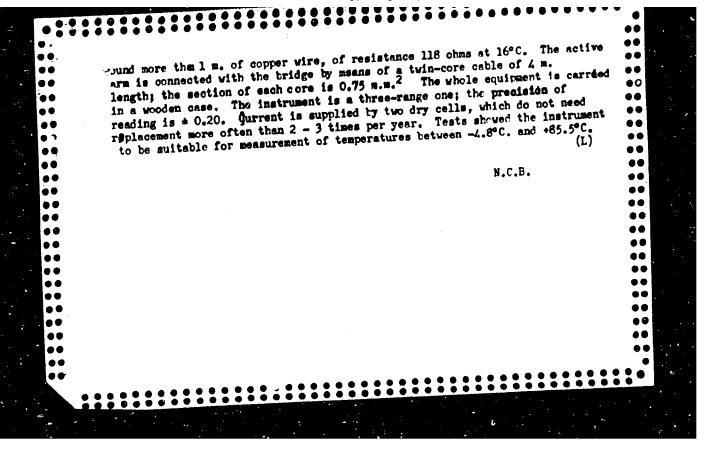
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Kraskovskii. S. A., O normal nom temperaturnom gradiente zemnol kory. [The normal temperature gradient of the earth's crust.] Vsesoiuznoe Geograficheskoe Obshchestvo. Izvestiia, 83(5):523-525, Sept.-Oct. 1951. 11 refs. DWB--An article questioning the correctness of the widely accepted theory evaluating the so-called mean temperature gradient of the earth's crust at 32 %km. Through a review of historical material, the suthor shows how this value of gradient originated and was adopted by science. First, he asserts that this mean value calculated according to values obtained by Cordier, Reich, Naumann, Everett, Prestowich, Thoma, Konigsberger (which were all different) and taken with aid of inert and Magnus geothermometers in bore holes made in sedimentary rocks is not precise and absolute, since overwelming accurate thermic material for all parts of the globe is now availabe. However, no complete analysis of this material has yet been made. The Use of a statistical method for obtaining the mean gradient, as applied by H. Landsberg at the University of Chicago in 1946-1947, without discounting geological conditions is, according to the author, incorrect. In general, the application of such a mean gradient obtained

in sedimentary rocks for celculating the thermic flow and solving other theoretical and practical problems is basically wrong. Such calculations can be made only on the basis of a "normal" gradient of the earth's crust, obtained by meansuring the temperature in crystalline rocks forming the structure of the earth's crust, but not in sedimentary rocks. Up to now the number of temperature measurements in crystalline rocks are not great but even these results show that the gradient in crystalline rocks differs much from the gradient of sedimentary series. All of them (gradients) lie in the interval between 6-18°/km. The normal gradient of the earth's crust will probably not surpass 10-12°/km, which is three times smaller than the value now prevailing. Subject Headings: L. Earth temperatures. 2. Temperature gradient. 3. U.S.S.R.—A.M.P.

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SOV/146-1-1-19/22

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ogical Sciences

TITLE: A.Beck; J.C.Jaeger and G.Newstead. The Measurement of the Thermal Conductivity of Rocks in Boreholes (Izmer-

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ABSTRACT: The paper discusses the article "The Measurement of the

Thermal Conductivities of Rocks by Observation in Boreholes", A.Beck, J.C.Jaeger and G.Newstead, Australian

Journal of Physics, 1956, Vol. 9, Nr 2, pp £86-£96, describes the device in question and its technical data.

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